



Enhancement of Alkaline Pressure Electrolysis System Performance

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AGENDA

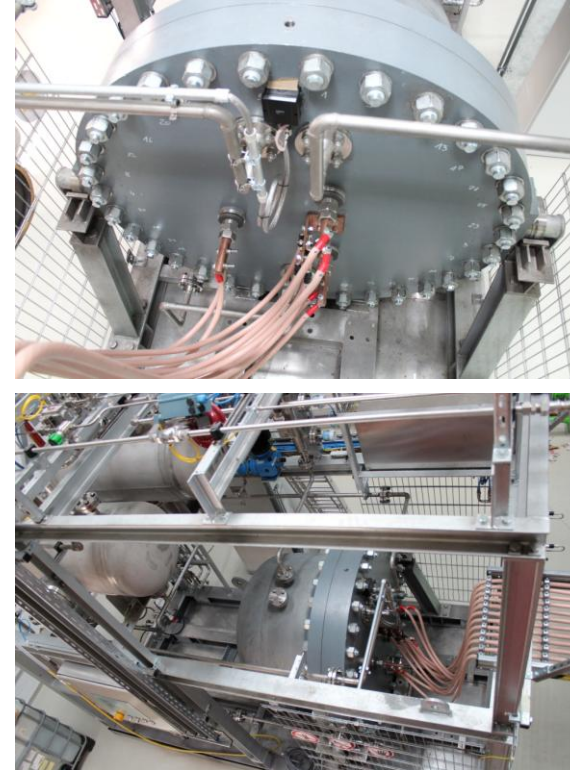
- 1 INTRODUCTION: PRESSURE ELECTROLYSIS AT THE HYDROGEN RESEARCH CENTER**
- 2 PRESSURE AND TEMPERATURE DEPENDENCE ON CELL VOLTAGE**
- 3 MEASUREMENT RESULTS**
- 4 ENERGETIC COMPARISON**
- 5 SUMMARY**



INTRODUCTION: PRESSURE ELECTROLYSIS

Research electrolyser

- 20 Nm³/h nominal hydrogen production rate
- 24 single cells – filter press design
- Operating pressure max. 58 bar
- Operating temperature 75 °C
- Current density up to 7.2 kA/m²
- Partial load 10 %
- Fast response time:
 - 50 A/s
 - ~ 60 s to max. power (warm stand-by)





INTRODUCTION: PRESSURE ELECTROLYSIS

Pressure vessel and stack

- External pressure vessel – filled with demineralised water
- Zirfon®-diaphragm
- Electrolyte:
Potassium hydroxide solution 28 wt.-%
- High efficient electrodes
 - Cathode: Raney nickel
 - Anode: Nickel
 - Perforated electrodes (0.44 m² each)

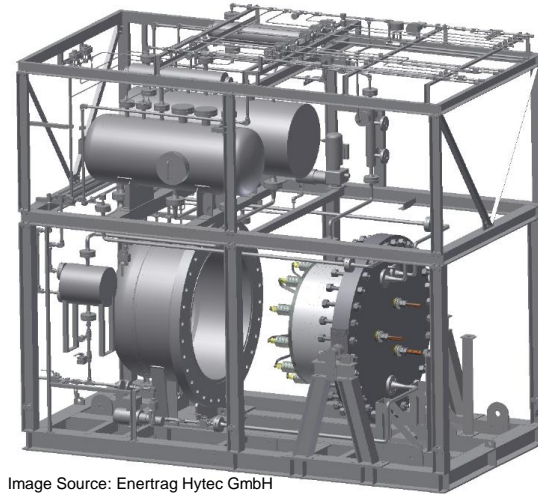


Image Source: Enertrag Hytec GmbH





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PRESSURE AND TEMPERATURE DEPENDENCE

Reversible cell voltage – temperature dependence

$$dG = -S dT + V dp$$

$$\frac{\partial \Delta_R G_m^0}{\partial T} = -\Delta_R S_m^0$$

$$\frac{\partial U_{rev}}{\partial T} = -\frac{1}{2F} \frac{\partial \Delta_R G_m^0}{\partial T} = \frac{\Delta_R S_m^0}{2F} = \frac{163.3 \text{ J K}^{-1} \text{ mol}^{-1}}{2 \cdot 96485 \text{ A s mol}^{-1}} = 0.846 \frac{\text{mV}}{\text{K}}$$

	Electrolysis of water
Reversible Cell Voltage	$\Delta U_{rev}^0 = -1.229 \text{ V}$
Entropy change	$\Delta S^0 = 0.1631 \text{ kJ K}^{-1} \text{ mol}^{-1}$
Temperature coefficient	0.85 mV K^{-1}

- Further temperature induced decrease of cell voltage by
 - Enhanced conductivity of electrolyte and membrane
 - Enhanced catalytic activity and exchange current density
 - Lower activation overpotential at electrodes



PRESSURE AND TEMPERATURE DEPENDENCE

Reversible cell voltage – pressure dependence

$$dG = -S dT + V dp$$

$$\frac{\partial \Delta_R G_m^0}{\partial p} = \Delta V_m^0$$

$$\frac{\partial U_{rev}}{\partial p} = -\frac{1}{2F} \frac{\partial \Delta_R G_m^0}{\partial p} = -\frac{\Delta V_m^0}{2F}$$

- Inserting ideal gas law and integration:

$$U_{rev}(p) = U_{rev}(p_0) - \frac{RT}{2F} \ln \left[\left(\frac{P_{H_2}}{P_0} \right) \left(\frac{P_{O_2}}{P_0} \right)^{1/2} \right] \quad (\text{valid for electrolysis of water, } H_2 \text{ and } O_2 \text{ pressurised})$$

	Electrolysis of water
Reversible Cell Voltage	$\Delta U_{rev}^0 = - 1.229 \text{ V}$
Pressure coefficient	- 44 mV/dec (at 25 °C)



PRESSURE AND TEMPERATURE DEPENDENCE

Reversible cell voltage – pressure dependence

- Assumption: only cathode side pressurised

$$\Delta U_{rev} = \frac{RT}{2F} \ln\left(\frac{P_{H_2}}{P_0}\right)$$

- Additional compression work

$$\Delta W = Q \times \Delta U_{rev} = n \times 2F \times \frac{RT}{2F} \ln\left(\frac{P_{H_2}}{P_0}\right) = nRT \ln\left(\frac{P_{H_2}}{P_0}\right)$$

→ Same work with ideal isothermal compression

→ Real compressor more scope to inefficiencies

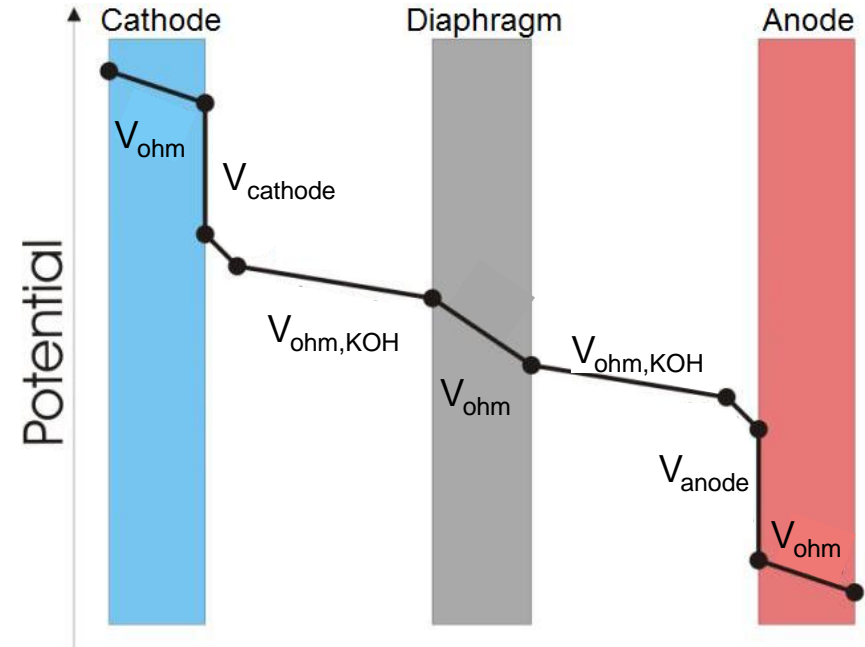
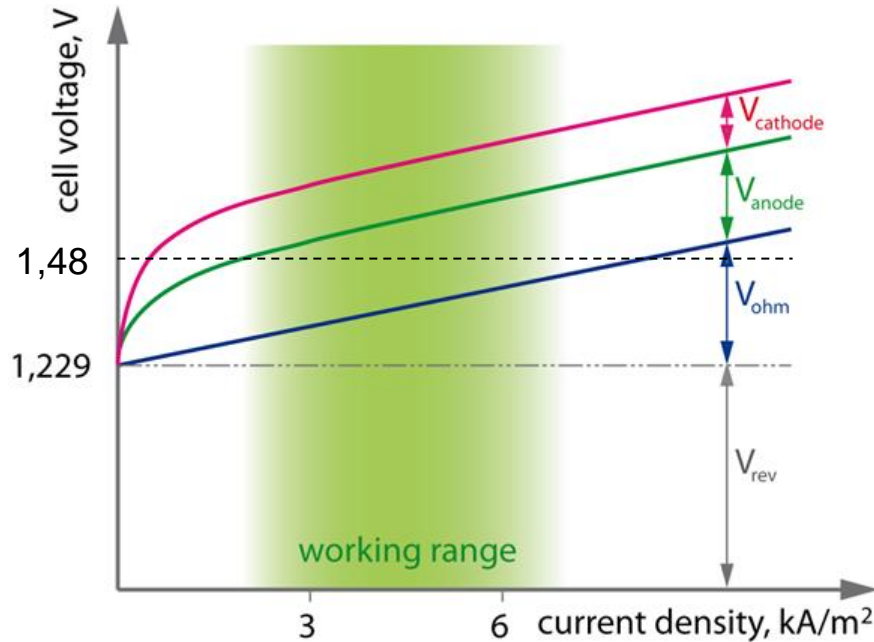
	Electrolysis of water
Pressure coefficient	- 30 mV/dec (at 25 °C)



PRESSURE AND TEMPERATURE DEPENDENCE

Overvoltages in real irreversible case

$$U_{cell} = U_{rev} + U_{an} + U_{cath} + U_{ohm}$$



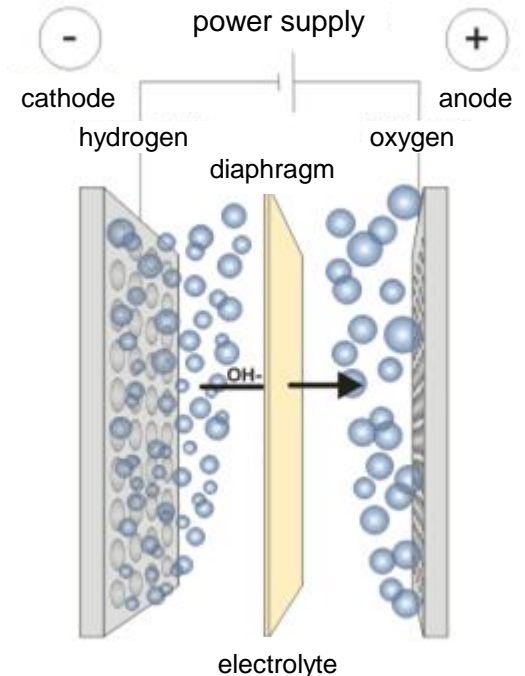


PRESSURE DEPENDENCE

Pressure electrolysis – bubble influence

Increasing pressure	
Positive influence	Negative influence
Decreasing bubble diameter → Decreasing ohmic resistance	Decreasing bubble diameter → Lower buoyancy force → Lower velocity of ascent → Bubbles stay longer in lye → More difficult to detach bubble from electrode surface

- To optimize
- Gap width (minimal resistance vs. optimal bubble flow)
- Gap geometry
- Surface morphology
- Flow velocity
- Avoid mass transport limitation (concentration overvoltage)
- Uniformity of current density





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MEASUREMENT RESULTS

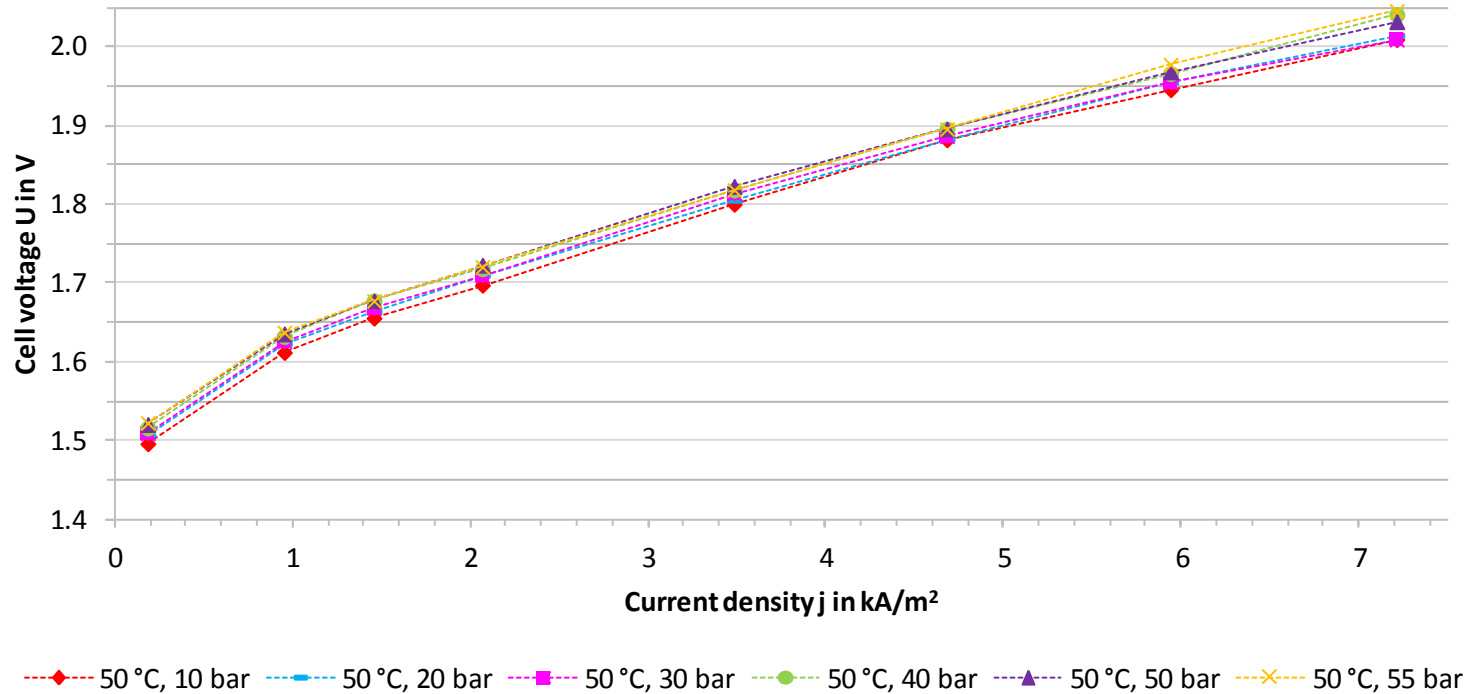
Measurement conditions

- Pressure: 10; 20; 30; 40; 50; 55 bar
- Temperature: 50; 60; 70 °C
- Current density: 0.18; 0.95; 1.46; 2.07; 3.48; 4.68; 5.94; 7.21 kA/m²
- Electrolyte flow rate constant at 800 l/h
- Residence time interval for each measurement: max. 5 min.
- No external cooling for minimal temperature difference between stack inlet and outlet
- Reference temperature: stack outlet, hydrogen site
- Cell voltage: mean value of series connection of 22 cells



MEASUREMENT RESULTS

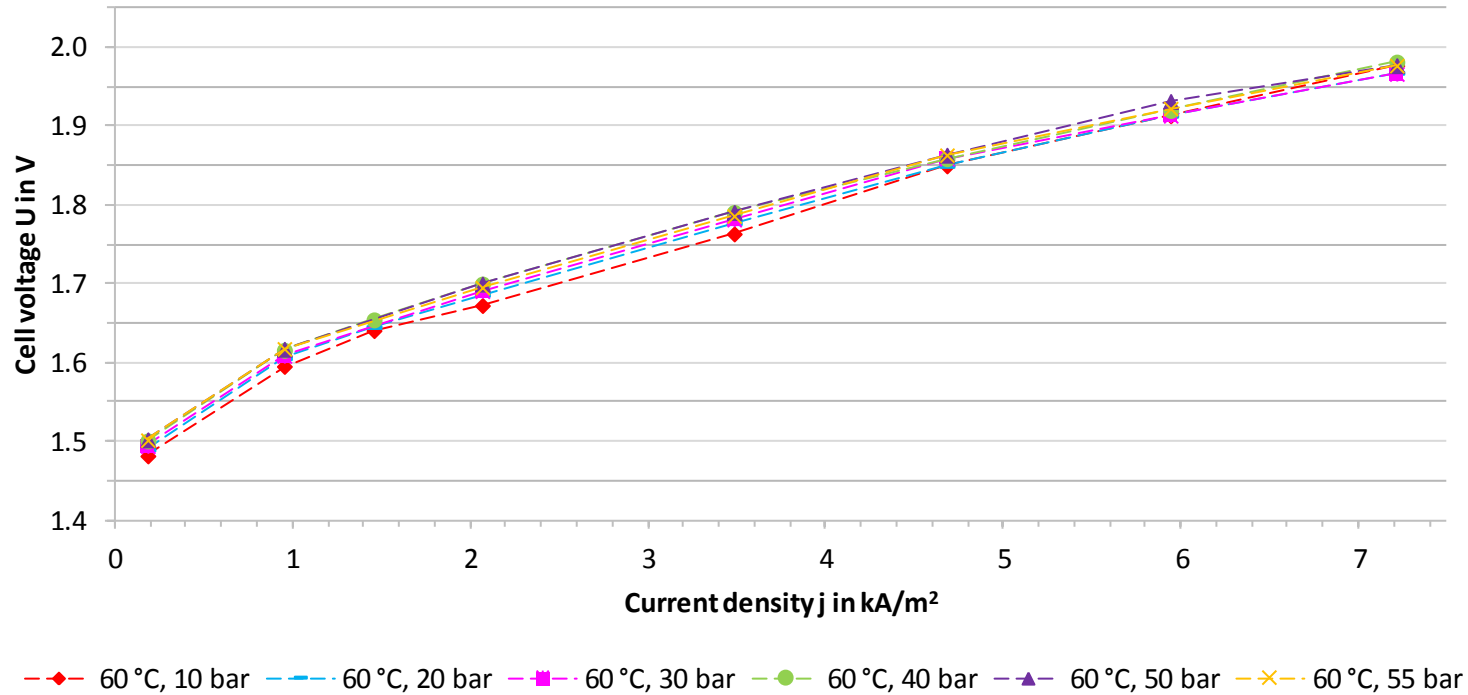
Pressure dependent j-U curve at 50 °C





MEASUREMENT RESULTS

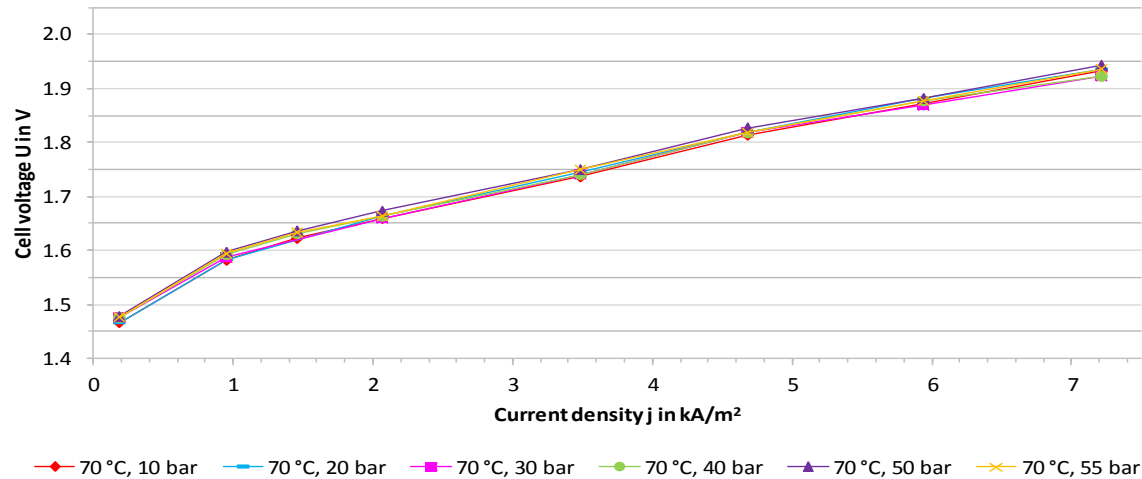
Pressure dependent j-U curve at 60 °C





MEASUREMENT RESULTS

Pressure dependent j-U curve at 70 °C



- Only marginal pressure influence on stack voltage for all temperatures and current densities

⇒ Slight increase of cell voltage

○ $(U_{55\text{bar}} - U_{10\text{bar}} \sim 0.02\text{V})$

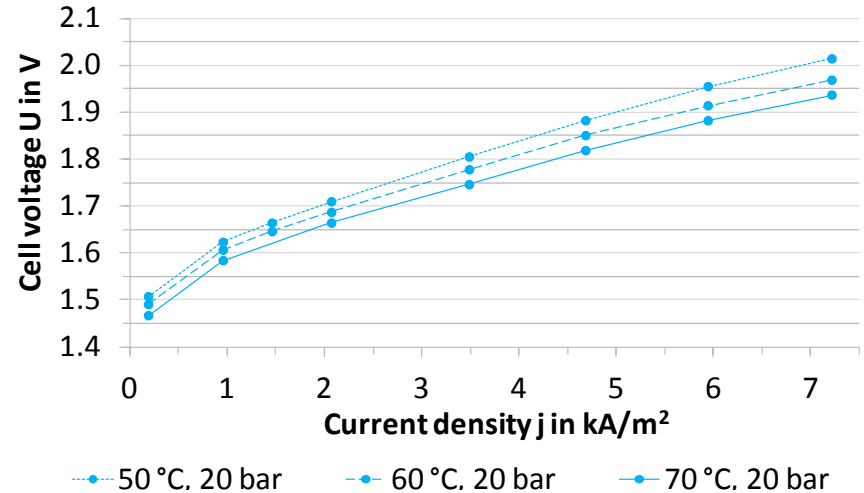
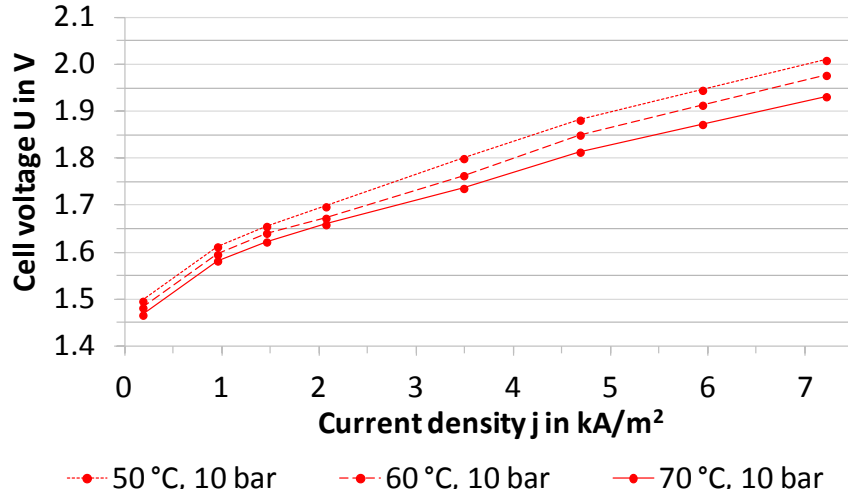
⇒ But decrease of cell overvoltage

○ 0.023 V



MEASUREMENT RESULTS

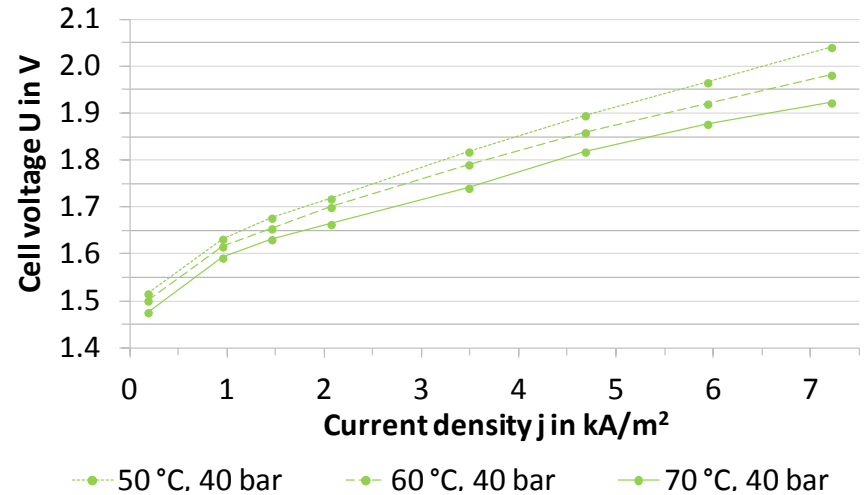
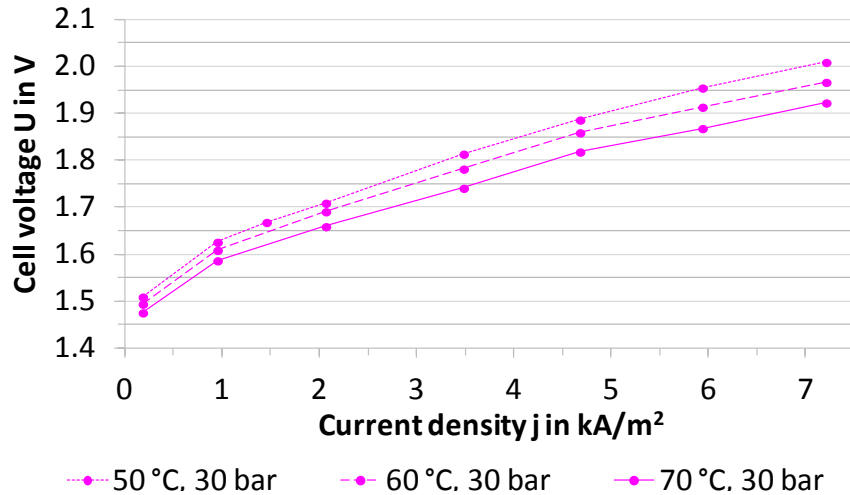
Temperature dependent j-U curves at 10 bar and 20 bar





MEASUREMENT RESULTS

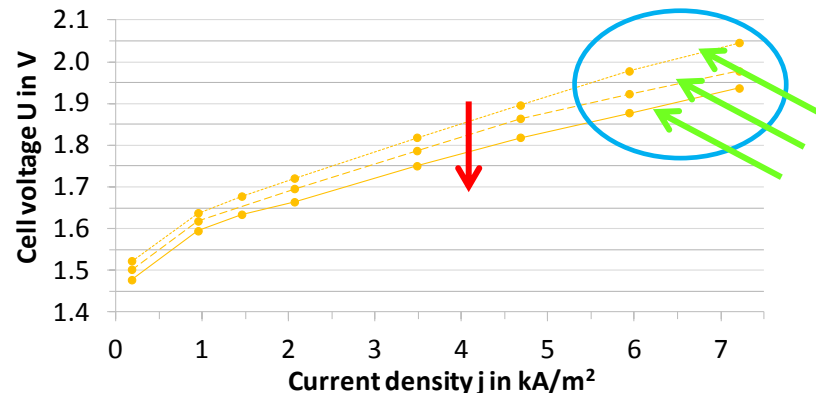
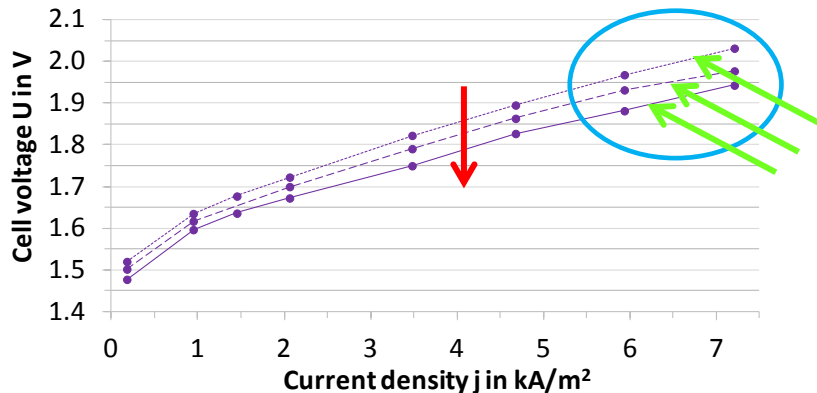
Temperature dependent j-U curves at 30 bar and 40 bar





MEASUREMENT RESULTS

Temperature dependent j-U curves at 50 bar and 55 bar



● 50°C, 50 bar ● 60°C, 50 bar ● 70°C, 50 bar

● 50°C, 55 bar ● 60°C, 55 bar ● 70°C, 55 bar

→ Significant temperature influence on cell voltage for all pressures and current densities

→ **Distinct decrease of cell voltage and cell overvoltage with temperature**

→ 1.9 mV/K (at 0.2 kA/m²) up to 4.6 mV/K (at 7 kA/m²)

→ Electrolyte resistance accounts for only one third of the temperature dependency

→ **Generally more pronounced at high current densities**

→ **Lower slope of the curves at higher temperatures**



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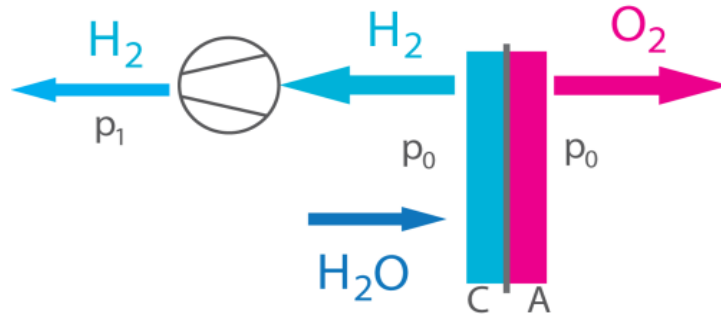
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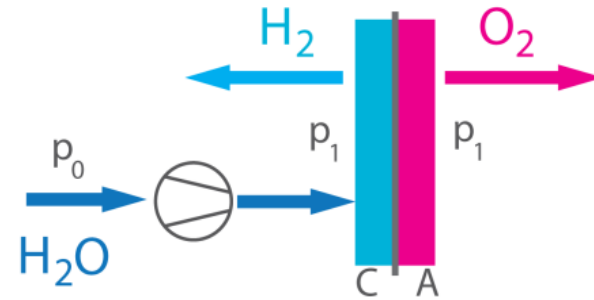
ENERGETIC COMPARISON

Atmospheric electrolysis vs. pressure electrolysis -1

Atmospheric electrolysis with subsequent compression



Pressure electrolysis with water boost pump



Practical approach for comparison:

- Because of practical independence of stack voltage from pressure we compare only additional energy for:

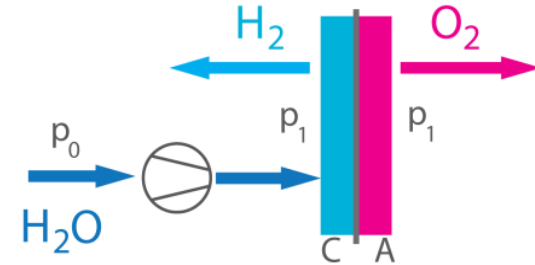
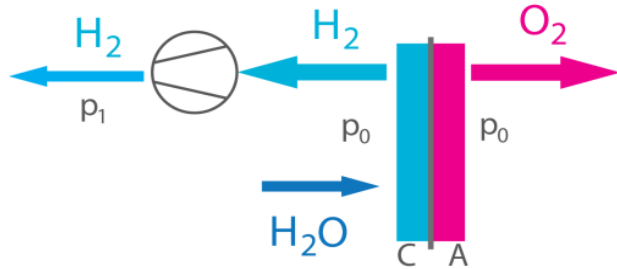
Hydrogen compression

water boost pump



ENERGETIC COMPARISON

Atmospheric electrolysis vs. pressure electrolysis - 2



Hydrogen compression

water boost pump

$$w_{compr} = \frac{w_{compr,rev}}{\eta_{mech} \cdot \eta_{isen}} = \frac{c_p \cdot m \cdot T_0}{\eta_{mech} \cdot \eta_{isen}} \left(\left(\frac{p_1}{p_0} \right)^{\frac{\kappa-1}{\kappa}} - 1 \right)$$

$$w_{pump} = p_1 \cdot \Delta V_{H_2O}$$

With $T_0 = 298 \text{ K}$, $\eta_{mech} = 0.98$, $\eta_{isen} = 0.75$
final pressure $p_1 = 60 \text{ bar}$:

$w_{compr} = 0.33 \text{ kWh}$

← per 1 m³ hydrogen (at STP) →

$w_{pump} = 0.014 \text{ kWh}$



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SUMMARY

- **Distinct temperature influence** on cell voltage
 - 1.9 mV/K (at 0.2 kA/m²) up to 4.6 mV/K (at 7 kA/m²)
 - Only one third of the influence caused by pure electrolyte conductivity
- Measurements: Only **marginal pressure influence** on cell voltage due to opposite effects
 - Result in coincidence with other authors
- Energetic comparison of pressure and atmospheric electrolysis
 - Atmospheric electrolysis: Hydrogen compressor $w_{compr} = 0.33 \text{ kWh/m}^3$
 - Pressure electrolysis: Water boost pump only $w_{pump} = 0.014 \text{ kWh/m}^3$
 - From this point of view **pressure electrolysis advantageous**



Thank you for your kind attention!



Image Source: Mercedes-Benz B-Klasse F-Cell

Chair of Power Plant Technology

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INTRODUCTION PRESSURE ELECTROLYSIS

System components

- Feed water system
- Cooling system
- Rectifier
- Gas drying and purification system

Pressure control systems

- Pressure balance control between H₂ and O₂ separators
- Pressure balance control between stack inside and surrounding

